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Supergiant Barocaloric Effects in Acetoxy Silicone Rubber over a Wide Temperature Range: Great Potential for Solid-state Cooling

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Electronic Supplementary Information

Abstract Solid-state cooling based on caloric effects is considered a viable alternative to replace the conventional vapor-compression refrigeration systems. Regarding barocaloric materials, recent results show that elastomers are promising candidates for cooling applications around room-temperature. In the present paper, we report supergiant barocaloric effects observed in acetoxy silicone rubber—a very popular, low-cost and environmentally friendly elastomer. Huge values of adiabatic temperature change and reversible isothermal entropy change were obtained upon moderate applied pressures and relatively low strains. These huge barocaloric changes are associated both to the polymer chain rearrangements induced by confined compression and to the first-order structural transition. The results are comparable to the best barocaloric materials reported so far, opening encouraging prospects for the application of elastomers in near future solid-state cooling devices.

Keywords Solid-state cooling; Barocaloric effect; Elastomer; Silicone rubber; Crystalline-amorphous transition

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INTRODUCTION

The current priorities in sustainability and energy efficiency lead to the study and development of new refrigeration technologies. In this context, solid-state cooling based on caloric effects (also called *i*-caloric effects^[1]) has shown to be a promising alternative to the conventional vapor-compression systems. The caloric effects can be described by an isothermal entropy change (ΔS_T) and an adiabatic temperature change (ΔT_S), both manifested when an external field is applied on a material. Depending on the nature of this external field (magnetic field, electric field, or stress field), the caloric effects can be categorized as magnetocaloric effect, electrocaloric effect, and mechanocaloric effect (σ -CE). The latter can still be divided in elastocaloric effect, driven by uniaxial stress, and barocaloric effect, driven by isotropic stress variations.

The first caloric effect reported was the elastocaloric effect in natural rubber (NR), observed by John Gough in the begin-

ning of the nineteenth century.^[2] Nevertheless, the research into caloric effects has strengthened only in the last two decades due to the discoveries of giant magnetocaloric effect in $\text{Gd}_5\text{Si}_2\text{Ge}_2$ compound^[3] and giant electrocaloric effect in $\text{PbZr}_{0.95}\text{Ti}_{0.05}\text{O}_3$ thin film.^[4] Even though σ -CE is the least researched among caloric effects, interesting results were reported for vulcanized natural rubber (VNR) and other synthetic elastomers already in the 1940 decade.^[5,6] Shape-memory alloys also exhibit promising σ -CE around room temperature.^[7–11] More recently, giant barocaloric effects were reported in $(\text{NH}_4)_2\text{SO}_4$ and molecular crystal below room temperature.^[12,13] Another promising class of material is plastic crystals, which demonstrated colossal barocaloric effects near room temperature.^[14,15] Regarding elastomers, the number of studies reporting large σ -CE values is gradually growing in the last years.^[16–23] On the contrary of what is observed in shape memory alloys and ionic salts, elastomers show significant elastocaloric and barocaloric effects even in the absence of phase transitions. This behavior is assigned to the rearrangement of polymer chains induced by the application of mechanical stress.^[16]

In this context, the silicone rubber can be considered a po-

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tential mechanocaloric material, since it is generally elastomeric and may present favorable structural transitions. The popular term “silicone” includes any organosilicon compound containing at least one pair of silicon atoms linked by an oxygen atom (Si—O—Si). Properly speaking, the correct terminology for these compounds is “polysiloxane”, whose formula is $(\text{RR}'\text{SiO})_n$, where R and R' are alkyl groups.^[24] Among the polysiloxanes, there is a group named room-temperature vulcanizing silicone rubbers (RTV-SR), which consist of polydimethylsiloxane, curing agent, fillers, and additives. Acetoxy silicone rubber (ASR) is a type of RTV-SR, which releases acetic acid during vulcanization. Recently, our preprint results^[25] motivated studies on ASR as a viable alternative for using as a refrigerant in solid-state devices based in barocaloric effects.^[26–28] In the present paper, we systematically investigate the barocaloric effect in ASR around room temperature. ΔS_T was evaluated following an indirect method using a Maxwell relation, and ΔT_S was directly measured. The results allowed us to establish a link between the crystalline-amorphous transition and the very large barocaloric changes observed in ASR.

EXPERIMENTAL

ASR samples were prepared by filling cylindrical plaster molds with a commercial silicone sealant resin (TYTAN Professional[®]) and were left to dry for approximately 24 h, to complete the room-temperature vulcanization process. For pressures up to 173 MPa, 12-mm-diameter samples were used; above 173 MPa, 8-mm-diameter samples were used. Both samples had length of ~20 mm and the average density was estimated by a pycnometer in $960 \text{ kg}\cdot\text{m}^{-3}$.

The experiments with pressure were performed in the experimental setup detailed elsewhere; the isostatic condition for barocaloric measurements was also discussed.^[20,21,23,29] Fig. S1 (in the electronic supplementary information, ESI), presents a schematic representation of the apparatus used in the barocaloric experiments. Two versions of the pressure chamber are available, consisting of carbon-steel cylinders with an 8 or 12 mm bore. The maximum pressure attainable with each chamber is 173 MPa (12 mm) and 390 MPa (8 mm). Samples are prepared in the proper shape to perfectly fit the chamber. A piston is the only movable part, responsible for compressing the sample. The bottom closure of the chamber has a narrow hole allowing a thermocouple to be placed inside the sample, monitoring its temperature. Another thermocouple, placed inside the chamber wall, monitors the chamber temperature, and its reading is used as a feedback to the temperature control system. A copper coil guides fluids (water or liquid nitrogen) around the chamber, and together with the heating elements, is responsible for controlling the chamber temperature. The chamber is placed on a load gauge and a hydraulic press actuates the piston. The pressure applied to the sample is directly given by the force measured by the load gauge divided by the piston cross-sectional area. A length gauge monitoring the displacement of the piston retrieves information about the deformation of the sample.

ΔT_S as a function of temperature (223–333 K) was directly

measured using a quasi-adiabatic compression/decompression process. In such process, pressure varies quickly enough to preclude significant heat exchange between the sample and its surroundings. Pressure changes between the minimum and the maximum pressures (p_1 and p_2 , respectively) were in the range of 26.0–390 MPa; compression corresponds to the process $p_1 \rightarrow p_2$, while decompression corresponds to the process $p_2 \rightarrow p_1$.

Strain versus temperature curves were measured at different constant pressures (0.9–332 MPa), varying the temperature at a rate of $\sim 3 \text{ K}\cdot\text{min}^{-1}$ for cooling and heating processes, within the 213–333 K temperature range. Strain (ϵ) is defined as $\epsilon(p, T) \equiv (l_{p,T} - l_0)/l_0$, where $l_{p,T}$ is the final length of the sample at pressure p , for each temperature T , and l_0 is its initial length measured at ambient pressure (p_0) and room temperature ($T_0 = 293 \text{ K}$). Since the cross-sectional area (A) of the samples does not vary in confined pressure, the volume change (ΔV) is directly proportional to the strain because $\epsilon(p, T) \equiv (A l_{p,T} - A l_0)/A l_0 = \Delta V/V_0$. These strain versus temperature curves up to 173(3) MPa were used in the calculation of ΔS_T versus T .

X-ray diffraction (XRD) patterns were measured at the XRD1 beamline,^[30,31] at the Brazilian Synchrotron Light Laboratory (LNLS). The beam energy used at XRD1 was 12 keV, and the samples were cooled down by a Cryojet5 (Oxford Instruments), within the 300–100 K temperature range at ambient pressure.

Fourier transform infrared spectroscopy (FTIR) was performed by a spectrometer from PerkinElmer[®] (model Spectrum Two), in the spectral range from 4000 cm^{-1} to 450 cm^{-1} , with spectral resolution of 1 cm^{-1} (Fig. S2, in ESI).

RESULTS AND DISCUSSION

In each ϵ versus T curves on heating process (Fig. 1a), one can see a narrow region where the derivative abruptly increases, and the transition temperature (T_{TR}) shifts toward higher temperatures for larger applied pressures. This behavior, in addition to the hysteresis shown in Fig. 1(b), strongly indicates a first-order transition. In fact, as observed in the XRD patterns (Fig. 1c), there is an amount of amorphous phase that becomes crystalline phase when the temperature decreases. To verify the influence of the pressure on T_{TR} , we calculated each T_{TR} from a local maximum in $d\epsilon/dT$ versus T curves. Considering a linear fit, we found $dT_{\text{TR}}/dp = 0.27(1) \text{ K}\cdot\text{MPa}^{-1}$ on heating and $0.23(1) \text{ K}\cdot\text{MPa}^{-1}$ on cooling (Fig. 1d).

Temperature as a function of time for ASR (see an example in Fig. 2a) was measured at the pressure range of 26.0(5)–390(12) MPa and different initial temperatures (223–333 K). The observed behavior is reversible in a large temperature range (*i.e.*, the adiabatic temperature change during compression and decompression is similar). The asymmetry found at the highest pressure in Fig. 2(a) (the absolute value of temperature change in decompression is higher than in compression for 390 MPa) is related to the partial amorphous-crystalline phase transition. In Fig. 2(b), ΔT_S corresponding to the decompression process is displayed. We observe a maximum barocaloric effect of 41.1 K, at $\sim 298 \text{ K}$, for $|\Delta p| = 390 \text{ MPa}$. This ΔT_S value, which we classify as supergiant ($|\Delta T_S|$

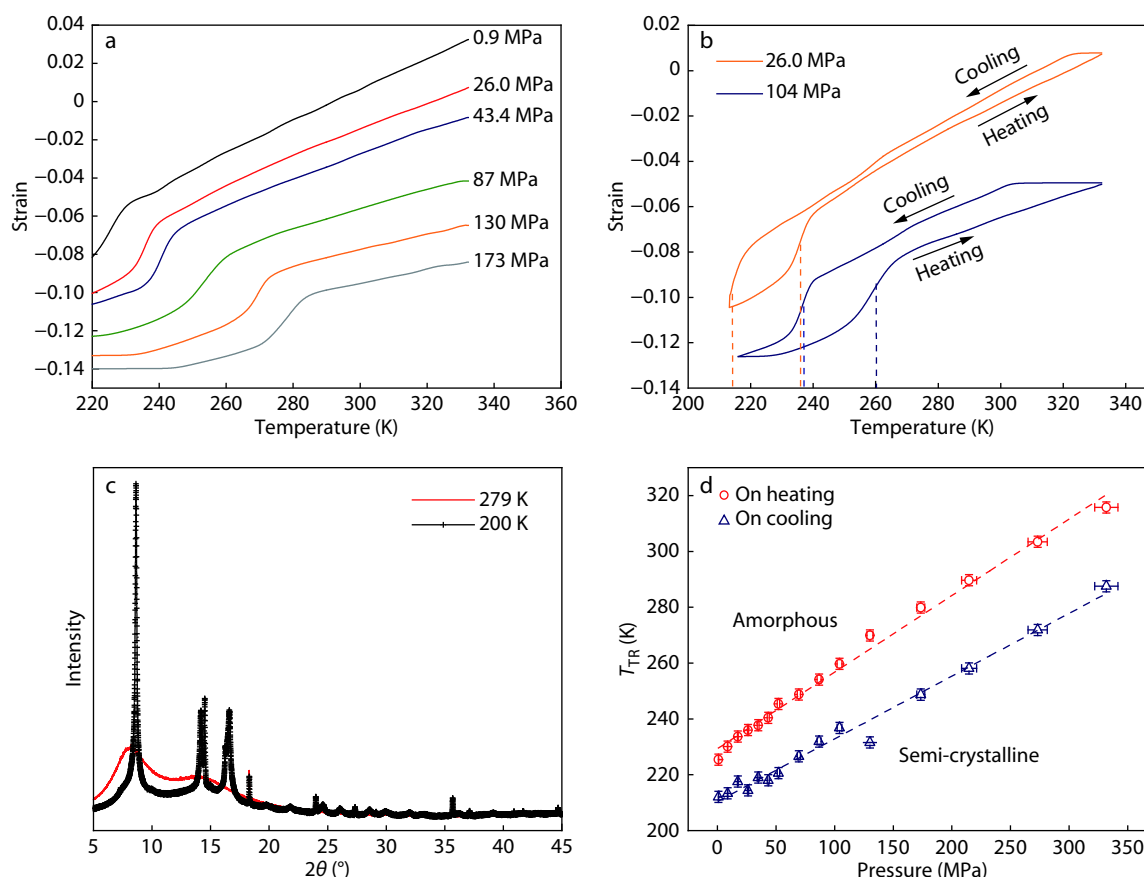


Fig. 1 (Color online) Crystalline-amorphous transition of ASR. (a) Strain versus temperature curves at constant pressures of 0.9(1), 26.0(5), 43.4(9), 87(2), 130(3), and 173(3) MPa measured on heating. (b) Strain versus temperature curves obtained in the cooling and heating processes, at 26.0(5) and 104(2) MPa; the vertical dash lines indicate the transition temperatures (T_{TR}), on heating and on cooling processes. (c) X-ray diffraction patterns corresponding to measurements at 279 K (amorphous phase) and 200 K (crystalline phase), at ambient pressure; see Fig. S3 and Table S2 (in ESI) for crystallographic information. (d) T versus p phase diagram: transition temperature on heating and on cooling processes versus applied pressure; open symbols are experimental data, and dash lines are the linear fits to obtain dT_{TR}/dp ; we estimate errors of $\pm 2\%$ for pressures up to 173 MPa and $\pm 3\%$ above 173 MPa, and ± 2 K for T_{TR} .

≥ 30 K), is significantly higher than those reported for any barocaloric materials around room temperature (e.g., VNR^[21] at ~ 315 K presents $|\Delta T_S| = 24.9$ K for $|\Delta p| = 390$ MPa; PDMS^[20] at ~ 283 K presents $|\Delta T_S| = 28.5$ K for $|\Delta p| = 390$ MPa). It is easy to see that a $|\Delta T_S|$ maximum appears for $|\Delta p| = 173$ MPa, and this maximum shifts to higher temperatures when the pressure increases. Considering a linear rate for the temperatures at the maximum ΔT ($T_{m,\Delta T}$) with pressure, we have $dT_{m,\Delta T}/dp = 0.22(8)$ K·MPa⁻¹. The outstanding ΔT_S values registered in ASR can be understood as a combination of the structural changes associated to the crystalline-amorphous transition and polymer chain rearrangements unrelated to phase transitions. Above $T_{m,\Delta T}$, the contribution to the barocaloric effect comes entirely from the amorphous phase. If we compare the $|\Delta T_S|$ values at $T_{m,\Delta T}$ with the $|\Delta T_S|$ values above $T_{m,\Delta T}$, an increase of 33%, 34%, and 47% is obtained for 173, 273, and 390 MPa, respectively. In addition, $|\epsilon|$ is less than 25% up to $|\Delta p| = 390$ MPa.

The ϵ versus T curves on heating and cooling processes were used to calculate ΔS_T as a function of temperature (Figs. 3a and 3b), according to Eq. (1), derived from Maxwell's

relation:^[19–21]

$$\Delta S_T(T, \Delta p) = -\rho_0^{-1} \int_{p_1}^{p_2} \left(\frac{\partial \epsilon_V}{\partial T} \right)_p dp \quad (1)$$

where ρ_0 is the density at p_0 and T_0 , and $p_1 \approx p_0$.

Taking ΔS_T on heating process as an example, the very large $|\Delta S_T|$ values were obtained, whose maxima are around 65(13), 100(20), 160(32), and 210(42) J·kg⁻¹·K⁻¹ for pressure changes of 26.0(5), 43.4(9), 87(2), and 173(3) MPa, respectively. The corresponding normalized entropy changes ($|\Delta S_T/\Delta p|$) are 2.5(6), 2.4(5), 1.8(4), and 1.2(3) kJ·kg⁻¹·K⁻¹·GPa⁻¹, respectively, which are much larger than those reported for PDMS^[20] and VNR.^[19,21] $|\Delta S_T|$ values increase more drastically due to the crystallization than ΔT_S discussed above. For instance, the $|\Delta S_T|$ value at the maximum for $|\Delta p| = 26.0$ MPa is more than twice the value in the amorphous region. For $|\Delta p| = 43.4$ MPa, we observe giant ΔS_T values at the amorphous region and supergiant ΔS_T ($|\Delta S_T| \geq 90$ J·kg⁻¹·K⁻¹) at the peak due to the structural transition. We observed that the temperature at the maximum $|\Delta S_T|$ ($T_{m,\Delta S}$) shifts to higher values when the pressure increases, increasing at a rate of $dT_{m,\Delta S}/dp = 0.26(3)$ K·MPa⁻¹, analogously to the maxima in $-\Delta T_S$ versus

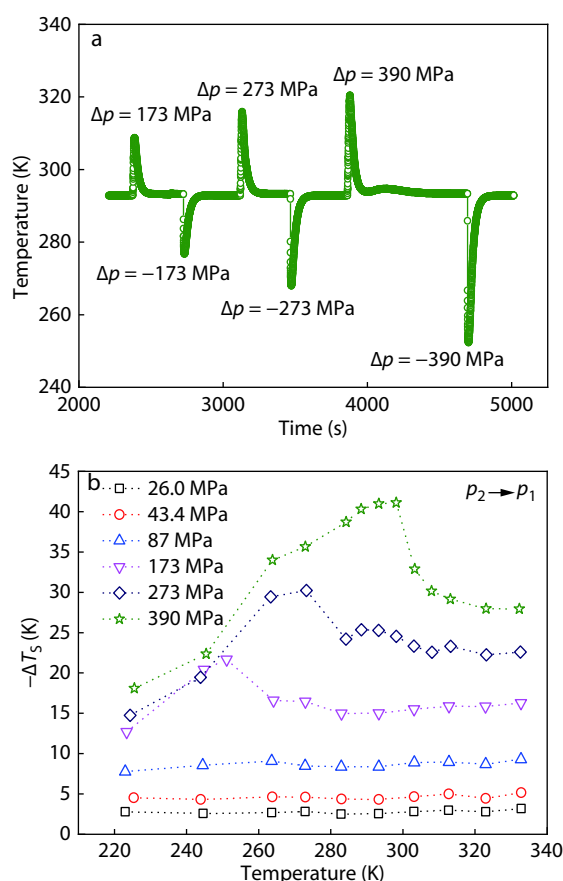


Fig. 2 (Color online) Adiabatic temperature change. (a) Temperature versus time for ASR during a barocaloric cycle at initial temperature of 293 K and pressure changes of 173(3), 273(8), and 390(12) MPa. (b) Adiabatic temperature change versus initial temperature for decompression process at different pressure variations; the dotted lines connecting the symbols are guides for the eyes; we estimate an error of $\pm 2\%$ for pressures up to 173 MPa and $\pm 3\%$ above 173 MPa, and an asymmetric error of $+4\%$ for $|\Delta T_S|$; p_1 and p_2 are the minimum and the maximum pressures, respectively.

T curves (Fig. 2b, $dT_{m,\Delta T}/dp = 0.22(8) \text{ K}\cdot\text{MPa}^{-1}$). Thus, ΔS_T and ΔT_S maxima shift similarly with pressure (taking the errors into account), although obtained from different processes. As expected, $dT_{m,\Delta S}/dp \cong dT_{TR}/dp$, since ΔS_T curves from Fig. 3(a) are obtained from ϵ versus T data on heating process. Similar behaviors can be observed taking ΔS_T on cooling process (Fig. 3b). Moreover, ΔS_T on heating and on cooling show irreversibility due to the hysteresis (*i.e.*, the difference between ΔS_T from heating and cooling processes cannot be negligible). In order to eliminate the irreversible contribution, the reversible ΔS_T as a function of temperature was estimated from the overlapping ΔS_T on heating and on cooling processes (Fig. 3c). We can see that the reversible $|\Delta S_T|$ is still supergiant (maximum of $182(46) \text{ J}\cdot\text{kg}^{-1}\cdot\text{K}^{-1}$ for $|\Delta p| = 173 \text{ MPa}$). This reversibility is essentially due to the amorphous phase. Regarding the peaks observed on Fig. 3, we must note that local fluctuations occur across the entire temperature and pressure ranges; such fluctuations are artifacts generated by the experimental and numerical precision of the

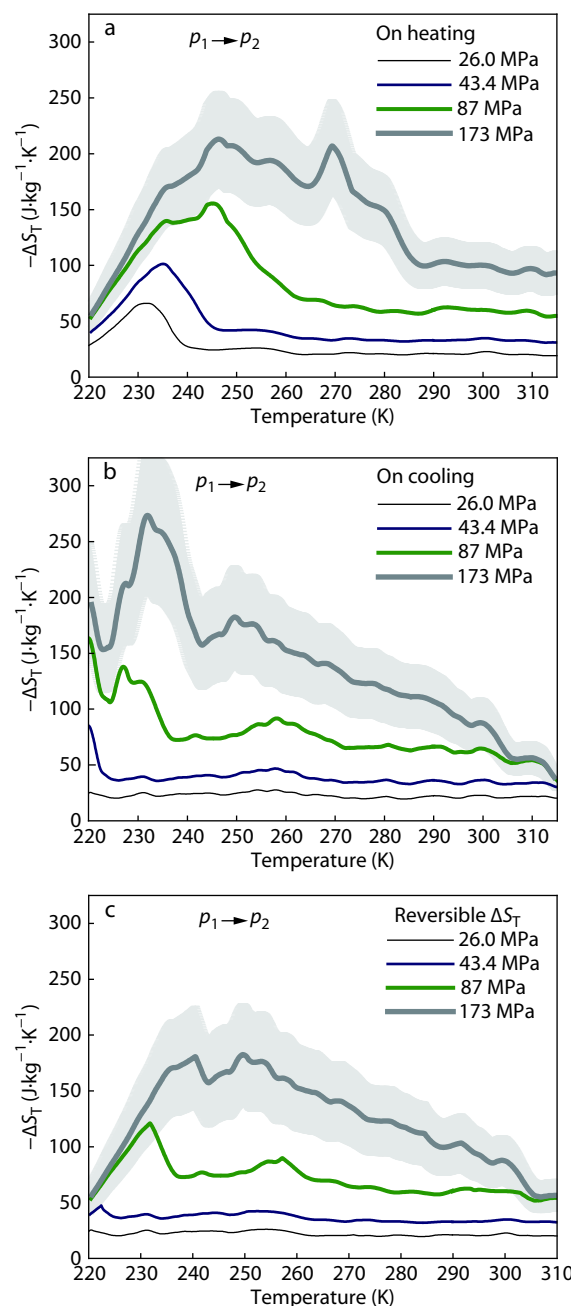


Fig. 3 (Color online) Isothermal entropy change. (a) Isothermal entropy change as a function of temperature for $|\Delta p| = 26.0(5)$, $43.4(9)$, $87(2)$, and $173(3) \text{ MPa}$, obtained from ϵ versus T data measured on heating process using Eq. (1); the errors were estimated in $\pm 20\%$. (b) Isothermal entropy change as a function of temperature for $|\Delta p| = 26.0(5)$, $43.4(9)$, $87(2)$, and $173(3) \text{ MPa}$, obtained from ϵ versus T data measured on cooling process using Eq. (1); the errors were estimated in $\pm 25\%$. (c) Reversible isothermal entropy change as a function of temperature for $|\Delta p| = 26.0(5)$, $43.4(9)$, $87(2)$, and $173(3) \text{ MPa}$, obtained from overlapping Figs. 3(a) and 3(b); the errors were estimated in $\pm 25\%$. The errors were only shown for 173 MPa (gray-filled area) for the sake of clarity. p_1 and p_2 are the minimum and the maximum pressures, respectively.

measurements and data analysis procedures.

Finally, we compared the barocaloric properties of ASR

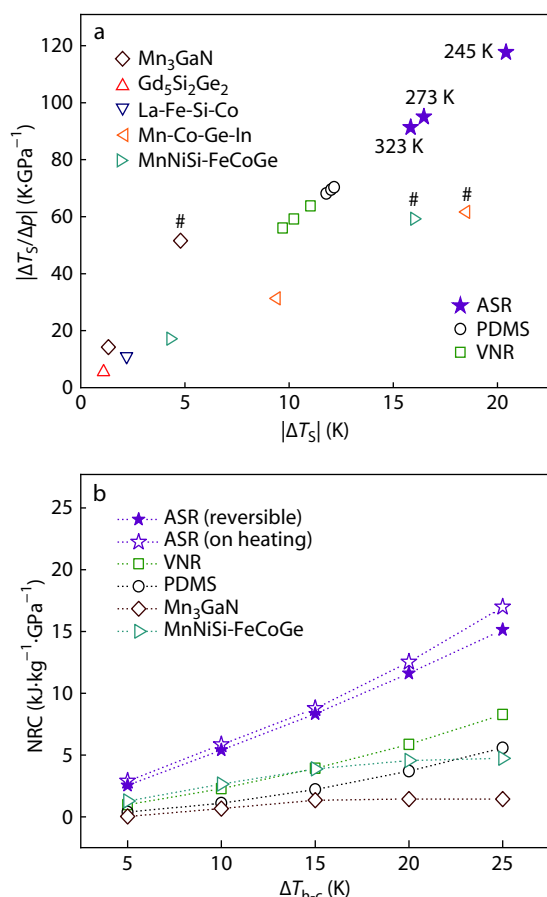


Fig. 4 (Color online) Performance parameters. (a) Normalized adiabatic temperature change versus temperature change for ASR ($|\Delta p| = 173$ MPa), PDMS ($|\Delta p| = 173$ MPa),^[20] VNR ($|\Delta p| = 173$ MPa),^[19,21] Mn₃GaN (maximum $|\Delta T_s|$ reported for $|\Delta p| = 93$ MPa),^[32] Gd₅Si₂Ge₂ (maximum $|\Delta T_s|$ reported for $|\Delta p| = 200$ MPa),^[33] La-Fe-Si-Co (maximum $|\Delta T_s|$ reported for $|\Delta p| = 200$ MPa),^[34] Mn-Co-Ge-In (maximum $|\Delta T_s|$ reported for $|\Delta p| = 300$ MPa),^[11] and MnNiSi-FeCoGe (maximum $|\Delta T_s|$ reported for $|\Delta p| = 250$ MPa);^[35] 245, 273, and 323 K are selected temperatures for ASR; # represents data obtained from indirect methods. (b) Normalized refrigerant capacity versus ΔT_{h-c} for ASR ($T_{\text{hot}} = 300$ K and $|\Delta p| = 173$ MPa; solid stars are related to reversible ΔS_T data and open stars are related to ΔS_T on heating), PDMS ($T_{\text{hot}} = 315$ K and $|\Delta p| = 130$ MPa), VNR ($T_{\text{hot}} = 315$ K and $|\Delta p| = 173$ MPa), Mn₃GaN ($T_{\text{hot}} = 295$ K and $|\Delta p| = 139$ MPa), and MnNiSi-FeCoGe ($T_{\text{hot}} = 335$ K and $|\Delta p| = 270$ MPa); the dotted lines connecting the symbols are guides for the eyes.

around room temperature with promising barocaloric materials in literature.^[9,11,19–21,32–35] The normalized adiabatic temperature change ($|\Delta T_s / \Delta p|$) as a function of $|\Delta T_s|$ is plotted in Fig. 4(a), where simultaneously larger $|\Delta T_s|$ and $|\Delta T_s / \Delta p|$ values indicate higher potential for barocaloric cooling applications. $|\Delta T_s / \Delta p|$ reaches a huge maximum value of ~ 120 K·GPa⁻¹ for $|\Delta T_s| = 20.4$ K. It is noteworthy the results for ASR exceed those of any other barocaloric material in a broad temperature range. We also calculated the normalized refrigerant capacity (NRC) as a function of the temperature difference between hot reservoir and cold reservoir ($\Delta T_{h-c} \equiv T_{\text{hot}} - T_{\text{cold}}$), following the equation:^[20,21]

$$\text{NRC}(\Delta T_{h-c}, \Delta p) = \left| \frac{1}{\Delta p} \int_{T_{\text{cold}}}^{T_{\text{hot}}} \Delta S_T(T, \Delta p) dT \right| \quad (2)$$

as shown in Fig. 4(b). For ASR, we fixed the hot reservoir at 300 K, $|\Delta p| = 173$ MPa and we used ΔS_T data from Fig. 3(a) and reversible ΔS_T data from Fig. 3(c). Again, the NRC values of ASR surpasses all barocaloric materials in the full ΔT_{h-c} range, and this difference increases as a function of ΔT_{h-c} , reaching ~ 15 kJ·kg⁻¹·GPa⁻¹ for $\Delta T_{h-c} = 25$ K. Moreover, the curve keeps a clear trend to increase, following a distinct behavior to that observed for the other non-elastomeric barocaloric materials in the comparison. Also, the relative cooling power ($\text{RCP} \equiv |\Delta S_{\text{max}} \times \delta T_{\text{FWHM}}|$, where ΔS_{max} is the maximum entropy change and δT_{FWHM} is the full width of the entropy change peak at half maximum) for ASR taking reversible ΔS_T is 13(3) kJ·kg⁻¹ for $|\Delta p| = 173(3)$ MPa; this RCP value is so huge that it exceeds all values reported for barocaloric materials by at least one order of magnitude.

CONCLUSIONS

Supergiant barocaloric changes are observed in ASR at moderate applied pressures and relatively low sample strains, reaching the maximum values of $|\Delta T_s| = 41.1$ K (at ~ 298 K, for $|\Delta p| = 390$ MPa) and reversible $|\Delta S_T| = 182(46)$ J·kg⁻¹·K⁻¹ for $|\Delta p| = 173$ MPa. The striking results for ASR also include a normalized adiabatic temperature change of ~ 120 K·GPa⁻¹ for $|\Delta T_s| = 20.4$ K and $|\Delta p| = 173$ MPa, a normalized refrigerant capacity of ~ 15 kJ·kg⁻¹·GPa⁻¹ for $\Delta T_{h-c} = 25$ K and $|\Delta p| = 173$ MPa, and a relative cooling power (RCP) of 13(3) kJ·kg⁻¹ for $|\Delta p| = 173$ MPa. The supergiant barocaloric values for ASR are due to combined effects of the first-order crystalline-amorphous transition and the polymer chain rearrangements unrelated to the crystallization process. These are the largest barocaloric effects known among elastomers so far. The major concern with elastomers is related to the low thermal conductivity, which can be improved by developing polymers with high conductivity fillers. But considering all the favorable characteristics exhibited by ASR concerning solid-state cooling, we can foresee a practical interest in the development of energy-efficient and environmental-friendly refrigeration devices based on barocaloric effect in polysiloxanes and other elastomers. As a further matter, pressure-induced crystallization on an amorphous polymer can dramatically modify its barocaloric properties; controlling or tuning the degree of crystallization in the barocaloric processes may lead to even greater values of ΔT_s , ΔS_T , refrigerant capacity, and relative cooling power.

NOMENCLATURE

ΔS_T	Isothermal entropy change
ΔT_s	Adiabatic temperature change
σ -CE	Mechanocaloric effect
NR	Natural rubber
VNR	Vulcanized natural rubber
RTV-SR	Room-temperature vulcanizing silicone rubbers
ASR	Acetoxy silicone rubber
PDMS	Polydimethylsiloxane
p	Pressure

ϵ	Strain
T	Temperature
$l_{p,T}$	Length of the sample at pressure p and temperature T
l_0	Length of the sample at ambient pressure and room temperature
A	Cross-sectional area of the sample
ΔV	Volume change
XRD	X-ray diffraction
FTIR	Fourier transform infrared spectroscopy
T_{TR}	Transition temperature
Δp	Pressure change
$T_{m,\Delta T}$	Temperature of the maximum ΔT
$T_{m,\Delta S}$	Temperature of the maximum ΔS
ρ_0	Density at ambient pressure and room temperature T
NRC	Normalized refrigerant capacity
ΔT_{h-c}	Temperature difference between hot and cold reservoirs
ΔT_{hot}	Temperature of the hot reservoir
ΔT_{cold}	Temperature of the cold reservoir
RCP	Relative cooling power
ΔS_{max}	Maximum entropy change
δT_{FWHM}	Full width of peak at half maximum

Electronic Supplementary Information

Electronic supplementary information (ESI) is available free of charge in the online version of this article at <https://doi.org/10.1007/s10118-020-2423-9>.

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